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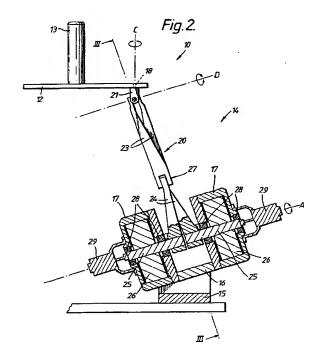
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(54) Actuator assembly.

© An actuator assembly (14) suitable for use in a hand controller (10) with six degrees of freedom of movement consists of a pair of arms (20) each secured at one end to a respective rotary actuator (26), and at the other end secured to a common universal joint (21). The arms (20) are coupled directly to the drive shafts (25) of the rotary actuators (26) and their movement is restricted.



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This invention relates to an actuator assembly and more specifically to an actuator assembly for use with a parallel platform structure such as a hand controller.

Parallel platform structures have found use in such applications as flight simulators, manipulators and hand controllers. These structures may typically be envisaged as having two triangular platforms: a top platform which is free to move in relation to a base platform which is fixed. These platforms are typically connected to each other at their corners via six linear actuators to form an octahedral structure. By altering the length of the linear actuators it is possible to locate the top platform in a variety of positions or orientations with respect to the base platform. Parallel platform structures of this type have a top platform which has six degrees of freedom of movement. However it is difficult to design parallel platform structures which have large working volumes using linear actuators, and it is also difficult to incorporate adequate back-drivability into these actuators. These problems are particularily acute when designing compact parallel platform structures. Pan tograph actuators which are operated by planetary geared motors have been proposed by H. Inoue et al as an alternative to linear actuators for use in parallel manipulators.

These pantograph actuators are of limited suitability for use in hand controllers due to their high torque noise which is a consequence of the use of a planetary gear mechanism. Also the varying inertia associated with different motor positions around the sun gear would be difficult to compensate for in a hand controller and would reduce its sensitivity. Also as the whole motor assembly is involved in the motion of any leg pair the effective inertia of the system is increased and sensitivity is again reduced. The inertia problems associated with planetary geared pantographic actuators make it difficult to provide the desired level of force feedback to devices incorporating these actuators. It is desirable that hand controllers are convenient to use and have adequate force feed back and back - drivability so as to minimize op erator fatigue.

According to the present invention these is provided an actuator assembly which comprises a pair of arms, each arm comprising upper and lower arm sections pivotally connected to each other, with said upper arm sections being joined at a three axis universal joint, and with said lower arm sections being attached independently of each other to a respective one of two rotary actuators, both rotary actuators being secured to a base via a common pivoting member.

According to a further aspect of the invention there is provided a hand controller which com-

prises three such actuator assemblies secured to a top plate via their three axis universal joints, the bases of the three actuator assemblies being spaced apart from each other.

The actuator assembly may be used in any application which requires a parallel platform structure with up to six degrees of freedom of movement. Such applications include flight sim—ulators, parallel manipulators, robotics and hand controllers. Hand controllers may be used to con—trol the movements of remote mechanisms such as manipulator slave arms, robots, remote vehicles and in such applications as the control of fly—by—wire aircraft.

The rotary actuators are preferably electrical direct drive motors. By direct drive it is meant that no gearing is involved in the operation of the motor so that the motor induces a direct response in the arm attached to its drive shaft. Most preferably the electrical direct drive motors are limited angle torque motors (LAT) such as brushless DC torque motors. These motors advantageously exhibit low magnetic and mechanical friction torque and very low reluctance and ripple torque, which results in a high quality force signal being generated from the actuator assembly. The use of direct drive limited angle torque motors produces an actuator assem – bly which is relatively compact but with a large working volume and improved force feedback.

It is preferred that the axis about which the pivoting member of an actuator assembly is able to pivot is perpendicular to but in the same or a parallel plane to the axis of rotation of the rotary actuators, this pivoting axis being stationary. It is preferred that the rotary actuators of an actuator assembly rotate about the same axis.

As the rotary actuators are located within a pivoting member attached to a base the actuator assembly mechanism is statically balanced in all positions in respect of the motor assemblies and at no time does motion of the actuator assembly involve displacements of the centre of mass of any pivoting member and the motors on it.

Preferably means are incorporated into the actuator assembly to enable it to communicate with and/or be controlled by the outside world. Such means include sensors and encoders which provide electrical signals which can be interpreted by for example a computer to identify the orientation of the actuator assembly and to control it.

Preferably means are incorporated in the hand controller to provide force feedback in relation to each degree of freedom of the handle. The fed – back forces and torques may be directly propor – tional to the forces exerted by corresponding joints of the mechanism being controlled, though to minimize operator fatique some forces exerted by the mechanism, such as those due to the weight of

an object being manipulated, or due to frictional effects in the joints, may be partially or completely filtered out.

Sensors in the hand controller provide electrical signals representing the forces or torques and the linear or angular displacements applied by the operator in each linear or rotary degree of freedom. These signals are desirably supplied to a computer, which provides corresponding control signals to motors in the mechanism being controlled. Different control modes may be selected during per formance of a task by an operator, for example: position control, rate control, or force control (displacement of the handle causing, respectively, a corresponding displacement of, rate of movement of, or force exerted by, the mechanism); and for each such mode of control the constants of proportionality might also be varied. For example for large - scale motions of the mechanism rate control might be used, to move the mechanism to where a task is to be performed, and then for fine-scale movements of the mechanism during performance of the task, position control with a 1:1 ratio might be preferred.

It is preferred that the encoders or sensors for the rotary actuators are coupled directly onto the drive shaft of the actuator rather than via an inter—mediate coupling. This ensures the highest stiff—ness coupling between the encoder and the drive shaft which allows for higher bandwidth control of the motor and for the construction of a more com—pact unit. Suitable encoders for direct coupling are the Heidenhain ERO series of encoders.

The invention will now be further described by way of example only, and with reference to the accompanying drawings, in which: -

Figure 1 shows a plan view of a hand controller including three actuator assemblies, but with all of the arms omitted for clarity;

Figure 2 shows a view, part in elevation and part in section of part of the hand controller of Figure 1 showing an actuator assembly including its arms; and

Figure 3 shows a view, part in elevation and part in section, of an actuator as - sembly as viewed along the line III - III of Figure 2.

Referring to Figure 1 there is shown a hand controller 10 which comprises a supporting plat—form 11 which is connected to a top plate 12, via three actuator assemblies 14. The top plate 12 carries a handle 13. Each actuator assembly 14 comprises a base 15 for supporting a pivoting yoke 16 which retains a pair of rotary actuators (not shown in Figure 1) which operate about an axis A and are located within respective actuator housings

17, a pair of pantograph arms (not shown in Figure 1) and a universal joint (not shown in Figure 1). Each actuator assembly 14 is secured to the sup – porting platform 11 via its base 15 such that each actuator assembly 14 is located at the vertex of an imaginary equilateral triangle and such that the axes A of the actuator assemblies 14 as seen in plan view intersect at the centre of the supporting platform 11. Each pivoting yoke 16 is able to pivot about an axis B, of each actuator assembly 14, in relation to the base 15 and supporting platform 11. The universal joints are secured to the top plate 12 at points 18.

Referring to Figure 2 and 3 there is shown an actuator assembly 14 of the hand controller 10 shown in Figure 1. A pair of pantograph arms 20 are attached to the top plate 12 by means of a universal joint 21. The universal joint possesses three rotational axes: C, D and E. The pantograph arms 20 possess upper and lower arm sections 23 and 24; the upper arm sections 23 are attached to and able to pivot about the axis D of the universal joint 21, while the lower arm sections 24 are fixed to respective driveshafts 25 of the pair of rotary actuators 26 such that they turn about axis A as the driveshafts 25 rotate. The upper and lower arm sections 23 and 24 of each pantograph arm 20 are pivotally connected to each other at point 27. The rotary actuators 26 are retained within the two actuator housings 17 which are attached to the pivoting yoke 16 secured to the base 15. The driveshafts 25 are supported by means of bearings 28 and are attached to encoders 29.

It will be apparent that the top plate 12 has six degrees of freedom of movement although its movement is somewhat restricted by the three actuator assemblies 14. The working volume of the hand controller 10 is related to the the angle of rotation about axis B of the pivoting yoke 16, the angles of rotation about axis A of the actuator driveshafts 25 and the relative angles between the upper and lower arm sections 23 and 24 of each pair of pantograph arms 20.

In operation of the hand controller 10 an oper – ator can move the handle 13 (and with it the top plate 12) with six degrees of freedom: linear dis – placements in three orthogonal directions, and ro – tations about three orthogonal axes. Any such movements cause changes in the orientations of at least one of the lower arm sections 24 relative to the respective yoke 16 and hence rotation of the corresponding driveshaft 25. Consequently the signals from the encoders 29 enable a computer (not shown) to determine at all times the position of the handle 13 and the movement to which it is subjected. The hand controller 10 with its asso – ciated computer can hence be used to control movement of, for example, a manipulator slave arm

(not shown). The forces and torques experienced by such a slave arm may be detected, and the operator can be provided with force (and torque) feedback by energising the rotary actuators 26 appropriately.

Claims

- An actuator assembly (14) which comprises a pair of arms (20), each arm comprising upper (23) and lower (24) arm sections pivotally connected to each other(27), with said upper arm sections (23) being joined at a three axis universal joint (21), characterised in that the lower arm sections (24) are attached indepen dently of each other to a respective one of two rotary actuators (26), both rotary actuators being secured to a base (15) via a common pivoting member (16).
- An actuator assembly as claimed in Claim 1 wherein the rotary actuators (26) are direct drive motors.
- An actuator assembly as claimed in Claim 2 wherein the direct drive motors are brushless DC torque motors.
- 4. A hand controller (10) which comprises three actuator assemblies (14) as claimed in any one of the preceding claims secured to a top plate (12) via their three axis universal joints (21), the bases (15) of the three actuator assemblies (14) being spaced apart from each other.

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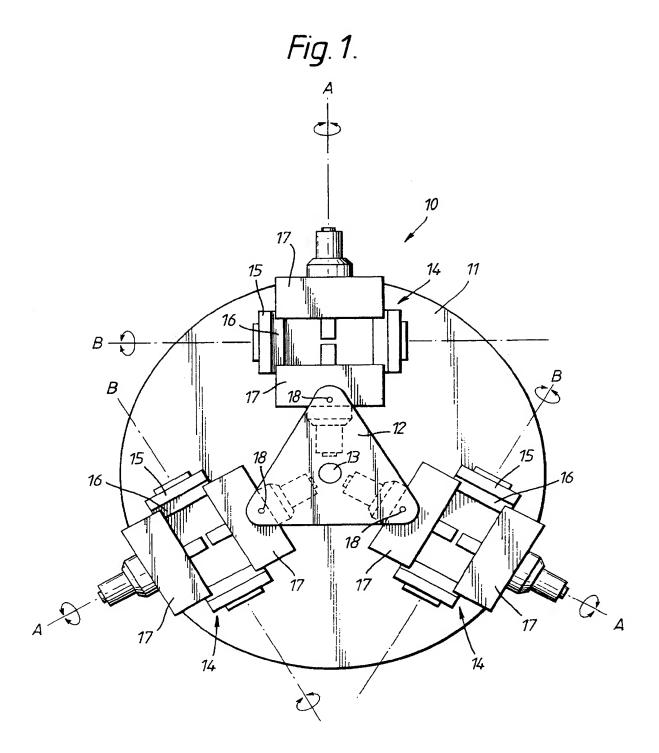
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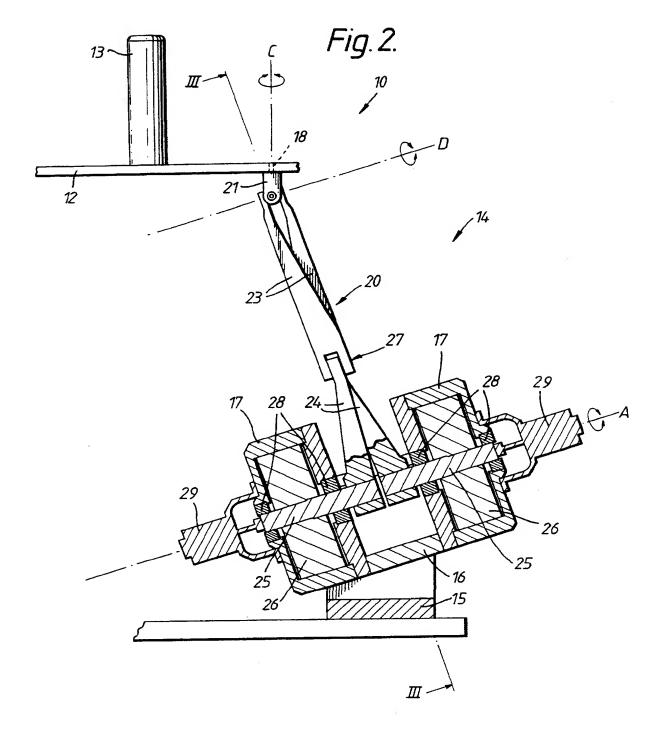
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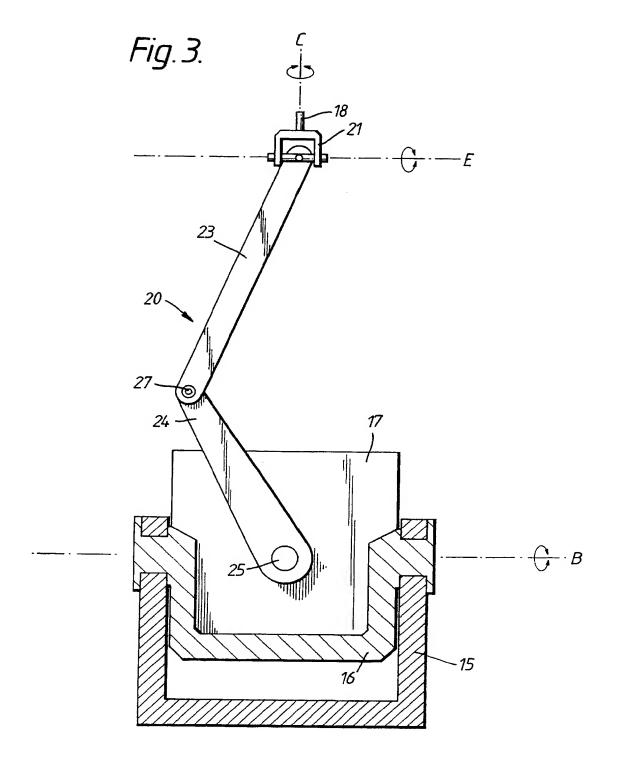
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EUROPEAN SEARCH REPORT

Application Number

EP 92 30 9175

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